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Copper/Solder Intermetallic Growth Studies

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1. Introduction

Intermetallic compounds (IMC's) have been identified as important elements in soldering. Aside from the currently mounting evidence of their role in solderability, they are also being proposed as having a significant impact on the mechanical properties of soldered materials. In this document we discuss some initial findings from a series of experiments regarding this IMC contribution to the changing physical properties of a solder joint, all as functions of time and temperature. In addition to the discussion of the initial experimental findings, we also present a working hypothesis about the relationship between intermetallic compounds and mechanical property considerations.

2. Experiment

2.1 Sample Preparation

Oxygen-free high-conductivity copper (OFHC) substrates were cleaned in room temperature solutions made from equal parts of 30percent ammonium hydroxide, 3-percent hydrogen peroxide, and deionized (DI) water. This immersion lasted for about 30 s. The samples were then rinsed in DI water followed by ethanol and finally blown dry. We then dipped the samples in a solder bath containing Kester ultra pure eutectic solder, held at 250°C, for about 30 s. The samples were then aged at 125°C for 59 days, providing reasonable thicknesses of both the Cu₆Sn₅ (eta phase) and Cu₃Sn (epsilon phase) intermetallics. After aging, the specimens were sectioned with a diamond saw and polished, finishing with 0.6-µm aggregate. Optical micrographs were produced and the IMC thicknesses were measured to be about 1 µm for the Cu₃Sn and 5 µm for the Cu_6Sn_5 (fig. 1). While no stains were used, polarizing filters helped distinguish the two IMC layers in the photomicrograph record made immediately following sample preparation.

2.2 Equipment

We performed the studies at ElectroScan Corporation of Wilmington, MA (Boston), using their recently introduced environmental scanning electron microscope (ESEM), which provides some unique features, including computer-controlled micro-positioning, 25 to 1000°C hot stage, and high pressure atmospheres (0 to 20 Torr) of nitrogen, H₂O, etc. These and other attributes allow emulation of real-world situations.

Figure 1. Optical micrograph—copper/solder interface immediately after aging and sample preparation and before ESEM.



2.3 Procedure

The sample was fixed in a 5-mm-diam ceramic crucible (part of the hot stage) using standard carbon paste and placed in the ESEM. We lowered the pressure of the specimen's chamber to about 4 Torr (the gas present was water vapor) and the temperature of the hot stage was ramped up, at a rate of about 10°C/min, to between 170°C and 180°C, and held there for about 2.5 hr. During this time a VCR film and a series of still images were recorded.

2.4 Images

In figures 2 through 7, the areas in the white boxes on the left side of the photographs are shown enlarged in the right half of the photographs, with the approximate temperature listed in the upper left corner.

The figures are listed in chronological order. Nearly 1.5 hr has elapsed between figures 2 and 7. All the images are of the cross-sectioned sample, reading from top to bottom in the figures: copper, intermetallic, and solder.

ESEM parameters listed along the bottom edge of the photograph are beam voltage, type of detector (secondary), magnification left image, magnification right image, working distance, and pressure (Torr). The next line down shows date and time. Figure 1 is a pho-

tomicrograph taken after sample preparation, with cross polarizers, making possible the differentiation of the two IMC's.

Figure 2. ESEM micrograph—copper/solder interface (time 0, arbitrarily chosen).

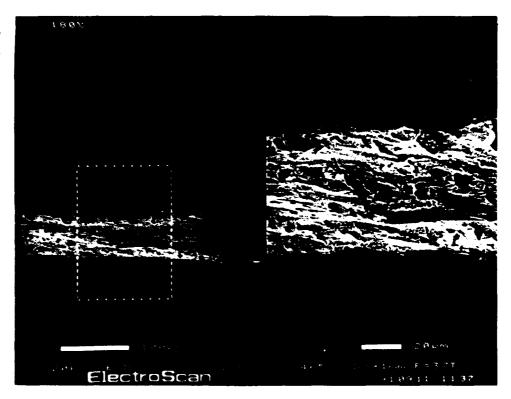


Figure 3. ESEM micrograph—copper/solder interface (Cu₃ clearly distinguishable from Cu₆Sn₅).

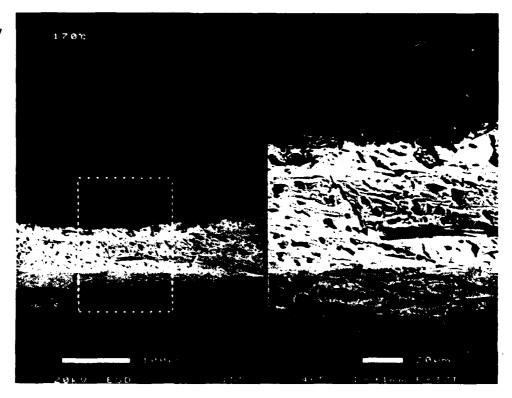


Figure 4. ESEM micrograph—copper/solder interface (time + 23 min).

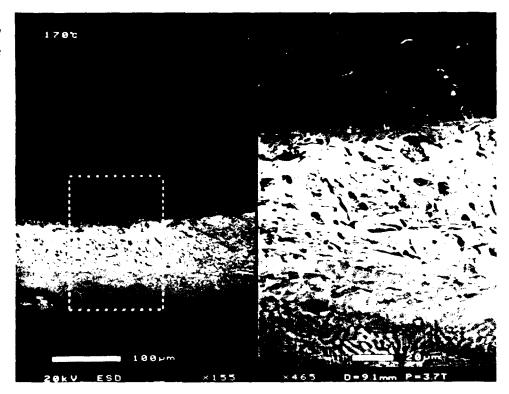


Figure 5. ESEM micrograph—copper/solder interface (time + 1 hr).

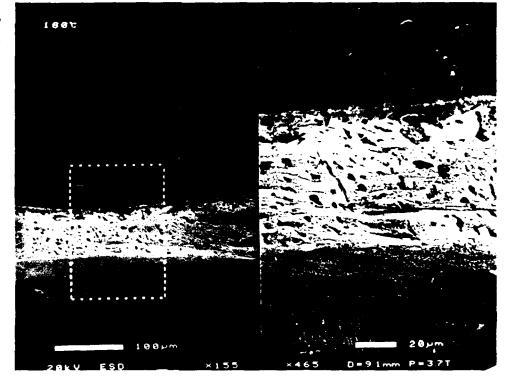


Figure 6. ESEM micrograph—copper/ solder interface (time + 1 hr 15 min).

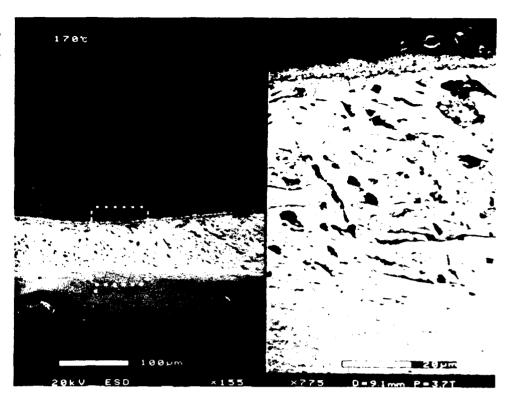
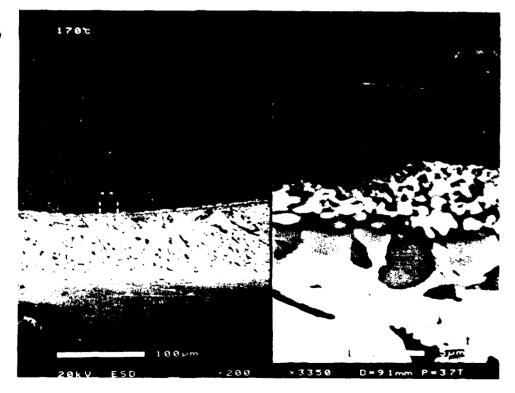


Figure 7. ESEM micrograph—copper, solder interface (extreme magnification—3350X—at time + 1 hr 27 min. Note out-of-plane growth of Cu₃Sn).



2.5 Observations and Remarks

Our most striking observation was that the Cu₂Sn showed the only signs of appreciable activity. The first signs of growth were small white flecks appearing at or near the Cu/Cu₃Sn interface (fig. 2). About the same time these flecks appeared, a slight roughening of the Cu₃Sn became apparent, making the two intermetallics distinguishable. This was followed by additional roughening of the Cu₃Sn, which was caused by the out-of-plane component of the Cu₃Sn's growth. It appeared that most of the grains grew at the same rate, making the field of them very regular in appearance (fig. 5 and 6). Over time the larger grains tended to be on the Cu₆Sn₅ rather than the Cu side of the Cu₃Sn (fig. 7). Also over time there was a difference in thickness (height out of plane) of the growing Cu₃Sn layer. The leading edge was thinner than the trailing edge (fig. 7). The question of whether all this activity might be just melting rather than growth behavior was answered by the fact that the melting points of all the constituents known to be present were above the sample temperature. Another concern was that the observed behavior might be the result of contamination. X-ray microanalysis showed potential contaminants to be below levels that could produce the results observed.

2.6 Followup Work

To assure that the results observed in the first set of experiments were not unique to that particular sample, we performed a second set of experiments, using a second specimen prepared and treated simultaneously with the first, but held aside and evaluated about a month later. Before working with the second sample, however, we verified calibration for the temperature of the ESEM hot stage by observing the controlled melting of pure elements. The accuracy of the stage was determined to be within 6°C across the range of interest (ambient to 175°C).

The second sample was treated in a similar fashion to the first as far as ramp rate, final temperature, gas pressure, gas species, and elapsed time. The same resulting changes and growth again appeared.

2.7. X-Ray Microanalysis

After ramp up, hold, and subsequent growth, we allowed the second sample to cool to near-ambient temperature, and while it was still within the chamber, we performed a series of energy-dispersive spectroscopy (EDS) analyses.

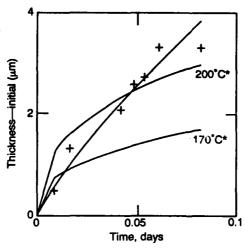
Spectra were first taken from the middle of the copper region and from a number of spots in the broad area of the solder. Next, successive spectra were taken stepping toward the IMC interfaces from the copper side and also from the solder side. These were designed to get a benchmark for the system and also to get a sense of the unwanted contributions to the spectra from neighbors. Finally, we chose a large but representative growth region and repeatedly probed areas of it; three spots were run two and three times each. The results showed that the analyses were reasonably well behaved. In particular, near-neighbor confounding of signals did not appear to be a problem.

Qualitative EDS showed the growth area to be composed of copper and tin. Quantitative standardless EDS produced atomic percent analyses that were within about 15 percent of those of Cu₃Sn.

3. IMC Growth

We evaluated the growth rates of the intermetallic layers by averaging the thicknesses of the layers over the cross section. This was done for the total IMC layer, the Cu₆Sn₅ (eta phase), and the Cu₃Sn (epsilon phase). For the total intermetallic layer, we compared the results to data published in *Solder Mechanics*. This relationship is illustrated in figure 8, and shows a higher and more linear growth of our total IMC layer than is shown in previously published data. Figures 9 and 10 illustrate the growth of the eta and epsilon phase layers, respectively. It can be seen that the eta layer thickness decreases in time, being consumed by the epsilon layer, which grows into the eta as well as the copper. Figure 11 shows the ratio of epsilon to eta

Figure 8. Comparison of total IMC growth to published data [1].



^{*}Plots of published data at 200°C and 170°C

¹D. R. Frear, W. B. Jones, and K. R. Kinsman, Solder Mechanics: A State of the Art Assessment, TMS-EMPMD Monograph Series, No. 1, Warrendale, PA (1991).

Figure 9. Cu_6Sn_5 growth with time.

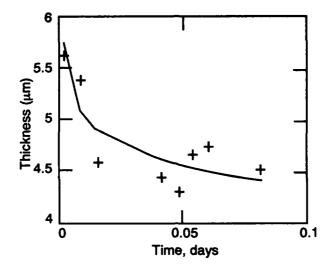


Figure 10. Cu₃Sn growth with time.

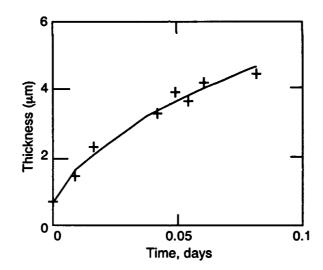
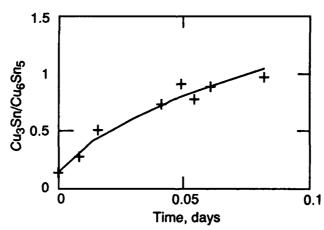


Figure 11. Ratio of Cu₃Sn thickness to Cu₆Sn₅ thickness as a function of time.



thickness in time and illustrates the increasing ratio of epsilon to eta. A percentage change in favor of the epsilon phase suggests a restriction of the tin supply to the interface region. Absolute movement of interfaces could not be determined since there were no markers placed in the cross section. All data gathering was performed at the surface of the sample. It is not known to what extent surface diffusion may have influenced the growth rates.

4. Hypothesis

The working hypothesis that is currently being examined proceeds as follows. The growth of the Cu_6Sn_5 nodule with long-term aging after reflow causes high strains in the solder bonded to the nodule's growth surface. The ductile Pb lamella deform with this growth and remain adhered, but the more brittle Sn lamella may actually debond. This debonding may be erratic because Sn properties vary widely in solder. With the reduced surface area caused by debonding, the diffusion of Sn from the bulk solder to the nodule is lowered. This serves as a self-limiting mechanism for the growth of the Cu_6Sn_5 nodule. With the reduction of the bulk Sn source, subsequent diffusion of Cu and the now limited Sn results in Cu_3Sn growth in two directions. First, Sn from the eta phase causes epsilon growth at the Cu interface. Second, Cu diffusing from the substrate causes additional epsilon to form at the eta/epsilon interface.

If the hypothesis is correct, the effect is a continual time degradation of electrical resistance, heat transfer, mechanical strength, and solderability at the IMC interface. Given that these parameters are critical to the reliability and maintenance of soldered components in the field, Cu₃Sn could be a critical parameter to detect and control in the manufacturing of electronic assemblies.

5. Future Research

The experiments should be repeated to establish a statistical basis for the results. Additional repetitions of our experiments should be conducted, in either an inert atmosphere or a vacuum, to eliminate corrosion or other environmental effects as potential contributors to the results. Relative bonding tendencies of Pb and Sn should be reviewed in the literature, by theory, or empirically. Higher magnification studies should be run primarily near areas of the more robust Cu₃Sn growth to look for the debonding phenomenon. Parametric monitoring should be included with future studies. For example, electrical resistance could be monitored as the Cu₃Sn growth pro-

ceeds. Finally, additional cross sectioning should be carried out to gather more bulk growth rate data to ascertain what relevant differences there are between the surface and bulk phenomena.

6. Conclusions

In our ESEM experiments, copper/tin intermetallic compounds were successfully observed to grow in copper/solder samples held at elevated temperatures. We made what we believe are the first movies of the growth of these intermetallics. A hypothesis was put forward suggesting that this growth could be detrimental to solder joint performance. Additional studies have been recommended to validate our preliminary results and test our hypothesis.

Acknowledgments

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